# A MUSCL finite volume scheme for axisymmetric compressible Euler equations

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22-26, June 2009

Porquerolles Workshop S. Clain, D. Rochette, R. Touzani

### Main motivation

- Numerical simulation of inductive plasma torches (ICP: Inductively Coupled Plasma Torch)
- This study is part of a TRP (Technology Research Program) with ESA (European Space Agency)

### Principle:

- A plasma torch is a quantitative chemical analysis technique (*e.g.* for detection of trace metals in environmental samples).
- It consists in ionizing a sample by injecting it in a plasma (generally in Argon): Atoms are ionized by a hot flame (6 000 to 8 000 K).
- The sample experiences fusion (solid), vaporization, and then ionization.
- High temperature is maintained by magnetic induction (thanks to a HF generator).
- lons are detected either by mass or emission spectrometry.

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# Summary

- A mathematical model for ICP
- Axisymmetric Euler equations
- A finite volume method
- MUSCL schemes
- Application to Euler equations
- Stationary radial solutions
- Numerical experiments

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## A mathematical model for ICP

Mathematical modelling of ICP takes into account various phenomena;

- Electromagnetic Induction: We use a quasi-static eddy current model (we neglect displacement currents). The major difficulty lies in the fact that an unknown part of the gas is transformed into plasma and becomes electrically conducting.
- Gas Dynamics: We are dealing with a compressible flow that we assume stationary and laminar.
- We use an axisymmetric description thanks to the device geometry.

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## 1. Electromagnetism

Eddy current equations read in quasi-static regime (time harmonic):

 $\begin{cases} \mathbf{curl} \, \mathbf{H} = \mathbf{J} \\ i \omega \mu_0 \mathbf{H} + \mathbf{curl} \, \mathbf{E} = 0 \\ \mathbf{J} = \sigma \, \mathbf{E} + \mathbf{J}_0 \end{cases}$ 

- J : Current density
- $J_0$  : Source current
- E : Electric field
- H : Magnetic field
- $\omega$  : Angular frequency
- $\sigma$  : Electric conductivity
- $\mu_0$  : Magnetic permeability of the free space

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#### We neglect here current transport by the fluid flow (In fact, we have $J = \sigma (E + u \times B) + J_0$ ).

In this model, we choose a formulation in terms of the electric field. We have

$$\begin{cases} \operatorname{curl}\operatorname{curl} \mathbf{E} + i\omega\mu_0\sigma\mathbf{E} = -i\omega\mu_0\mathbf{J}_0 & \text{ in } \mathbb{R}^3\\ |\mathbf{E}(\mathbf{x})| = \mathcal{O}(|\mathbf{x}|^{-1}) & |\mathbf{x}| \to \infty \end{cases}$$

where  $\sigma = \sigma(e)$  with

$$\sigma(e) = egin{cases} 0 & ext{if } e \leq e_0, \ > 0 & ext{otherwise} \end{cases}$$

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# 2. Flow of gas-plasma

We use compressible Euler equations (we neglect viscosity and thermal diffusion) with the following features:

- The gas motion is driven by the Lorentz force that we average on a time period.
- The energy source is given by Joule heating (also time averaged).

$$\nabla \cdot (\rho \,\mathbf{u} \otimes \mathbf{u}) + \nabla \rho = \rho \,\mathbf{g} + \frac{\mu_0}{2} \operatorname{Re} \left(\mathbf{J} \times \overline{\mathbf{H}}\right)$$
$$\nabla \cdot (\rho \,\mathbf{u}) = 0$$
$$\nabla \cdot \left(\left(E + \rho\right) \mathbf{u}\right) = \frac{1}{2} \operatorname{Re} \left(\mathbf{J} \cdot \overline{\mathbf{E}}\right) - R$$
$$\rho = \rho(\rho, e)$$

where **u** is the velocity,  $\rho$  is the pressure,  $\rho$  is the density, **g** is the gravity vector, e is the interna specific energy and E is the total energy defined by  $E = \rho \left(e + \frac{1}{2} |\mathbf{u}|^2\right)$ , R is a radiation source.

In the following, we restrict the model to an ideal gas

 $p = (\gamma - 1) 
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## **Axisymmetric Euler equations**

- We consider compressible time dependent Euler equations.
- The geometry of the domain suggests using an axisymmetric model.
- We don't take into account, in the sequel, sources (Joule and Lorentz)

Let  $(r, \theta, z)$  stand for cylindrical coordinates and let  $(u_r, u_\theta, u_z)$  stand for the components of a vector in this system, we obtain the system of equations (taking into account  $\theta$ -invariance):

$$\frac{\partial}{\partial t}(r\rho) + \frac{\partial}{\partial r}(r\rho u_r) + \frac{\partial}{\partial z}(r\rho u_z) = 0$$
  
$$\frac{\partial}{\partial t}(r\rho u_r) + \frac{\partial}{\partial r}(r\rho u_r^2 + r\rho) + \frac{\partial}{\partial z}(r\rho u_r u_z) = \rho u_{\theta}^2 + \rho$$
  
$$\frac{\partial}{\partial t}(r\rho u_z) + \frac{\partial}{\partial r}(r\rho u_r u_z) + \frac{\partial}{\partial z}(r\rho u_z^2 + r\rho) = 0$$
  
$$\frac{\partial}{\partial t}(r\rho u_{\theta}) + \frac{\partial}{\partial r}(r\rho u_{\theta} u_r) + \frac{\partial}{\partial z}(r\rho u_{\theta} u_z) = -\rho u_{\theta} u_r$$
  
$$\frac{\partial}{\partial t}(rE) + \frac{\partial}{\partial r}(ru_r(E + \rho)) + \frac{\partial}{\partial z}(ru_z(E + \rho)) = 0$$
  
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$$\begin{aligned} \frac{\partial}{\partial t}(r\rho) &+ \frac{\partial}{\partial r}(r\rho u_r) + \frac{\partial}{\partial z}(r\rho u_z) = 0\\ \frac{\partial}{\partial t}(r\rho u_r) &+ \frac{\partial}{\partial r}(r\rho u_r^2 + r\rho) + \frac{\partial}{\partial z}(r\rho u_r u_z) = \rho u_{\theta}^2 + \rho\\ \frac{\partial}{\partial t}(r\rho u_z) &+ \frac{\partial}{\partial r}(r\rho u_r u_z) + \frac{\partial}{\partial z}(r\rho u_z^2 + r\rho) = 0\\ \frac{\partial}{\partial t}(r\rho u_{\theta}) &+ \frac{\partial}{\partial r}(r\rho u_{\theta} u_r) + \frac{\partial}{\partial z}(r\rho u_{\theta} u_z) = -\rho u_{\theta} u_r\\ \frac{\partial}{\partial t}(rE) &+ \frac{\partial}{\partial r}(ru_r(E + \rho)) + \frac{\partial}{\partial z}(ru_z(E + \rho)) = 0\\ \rho &= (\gamma - 1)\rho e\end{aligned}$$

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We can write this system under the conservative formulation:

$$\frac{\partial}{\partial t}(rU) + \frac{\partial}{\partial r}(rF_r(U)) + \frac{\partial}{\partial z}(rF_z(U)) = G(U)$$

where

$$U = \begin{pmatrix} \rho \\ \rho u_r \\ \rho u_z \\ \rho u_\theta \\ E \end{pmatrix}, \ F_r(U) = \begin{pmatrix} \rho u_r \\ \rho u_r^2 + \rho \\ \rho u_z u_r \\ \rho u_\theta u_r \\ u_r(E + \rho) \end{pmatrix}, \ F_z(U) = \begin{pmatrix} \rho u_z \\ \rho u_r u_z \\ \rho u_r^2 + \rho \\ \rho u_\theta u_z \\ u_z(E + \rho) \end{pmatrix}, \ G(U) = \begin{pmatrix} 0 \\ \rho u_\theta^2 + \rho \\ 0 \\ -\rho u_\theta u_r \\ 0 \end{pmatrix}$$

This formulation involves a divergence form that can be discretized by finite volumes, source terms being treated separately.

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## A finite volume method

Consider a triangulation of the domain  $\Omega$  of parameters (r, z). Let:

- $-T_i$ : Triangle,  $1 \le i \le n_T$
- $e_{ij}$ : Common edge to triangles  $T_i$  and  $T_j$
- $-\mathbf{n}_{ij} = (n_{ij,r}, n_{ij,z})$ : Unit normal to the triangle  $T_i$  oriented toward  $T_j$
- $-\nu(i)$ : Index set of the (3) neighbour triangles of  $T_i$

Let us integrate the system of equations over a triangle  $T_i$  and use the divergence theorem. We get

$$\frac{d}{dt}\int_{\mathcal{T}_i} U(r,z,t) \, r \, dr \, dz + \int_{\partial \mathcal{T}_i} (F_r(U)n_{ij,r} + F_z(U)n_{ij,z}) \, r \, d\sigma = \int_{\mathcal{T}_i} G(U) \, dr \, dz$$

Let  $(t^n = n \, \delta t)_{n \in \mathbb{N}}$  denote a uniform subdivision of the interval  $[0, \infty)$ . We have

$$\int_{T_i} U(r, z, t^{n+1}) r \, dr \, dz = \int_{T_i} U(r, z, t^n) r \, dr \, dz$$
$$- \int_{t^n}^{t^{n+1}} \int_{\partial T_i} (F_r(U) n_{ij,r} + F_z(U) n_{ij,z}) r \, d\sigma \, dt$$
$$+ \int_{t^n}^{t^{n+1}} \int_{T_i} G(U) \, dr \, dz \, dt$$

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and define the approximation

$$U_i^n \approx \frac{1}{|T_i|_r} \int_{T_i} U(r,z,t^n) r \, dr \, dz.$$

We consider the approximate flux:

$$F_{ij}^{n} \approx \frac{1}{\delta t |e_{ij}|_{r}} \int_{t^{n}}^{t^{n+1}} \int_{e_{ij}}^{t^{n+1}} (F_{r}(U)n_{ij,r} + F_{z}(U)n_{ij,z}) r \, d\sigma \, dt$$

and the source term

$$G_i^n pprox rac{1}{\delta t |\mathcal{T}_i|} \int_{t^n}^{t^{n+1}} \int_{\mathcal{T}_i} G(U) \, dr \, dz \, dt.$$

We the define the scheme:

$$|T_i|_r U_i^{n+1} = |T_i|_r U_i^n - \delta t \sum_{j \in \nu(i)} |e_{ij}|_r F_{ij}^n + \delta t |T_i| G(U_i^n) \qquad 1 \le i \le n_T.$$

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The finite volume scheme is entirely determined by the choice of  $F_{ij}^n$  and  $G_i^n$ . For instance, the Rusanov scheme consists in defining the flux:

$$F_{ij}^{n} = \frac{1}{2} (F_{r}(U_{i}) + F_{r}(U_{j}))n_{ij,r} + \frac{1}{2} (F_{z}(U_{i}) + F_{z}(U_{j}))n_{ij,z} - \lambda_{ij}(U_{j} - U_{i})$$

#### where $\lambda_{ij}$ is large enough to ensure stability.

Other alternative schemes:

- Godunov: It consists in solving exactly the obtained Riemann problems.
- HLL (Harten, Lax, Van Leer): Approximate solution of Riemann problems.
- HLLC (+ Contact): Adaptation of HLL to contact discontinuities.

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# A second-order scheme (MUSCL)

- The first MUSCL scheme (*Monotonic Upwind Scheme for Conservation Laws*) is due to Van Leer ('79) for the 1-D case.
- There exist a variety of extensions to the multidimensional case.
- T. Buffard, S. Clain and V. Clauzon have proposed a new extension based on the calculation of directional derivatives.

We present an extension to the axisymmetric case.

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#### Consider the conservation law:

$$\frac{\partial u}{\partial t} + \frac{\partial}{\partial x}f(u) = 0 \qquad x \in \mathbb{R}, \ t > 0$$

The basic finite volume scheme uses a piecewise constant approximation. For instance, the first-order upwind scheme reads:

$$\frac{du_i}{dt} + \frac{f(u_i) - f(u_{i-1})}{\delta \times} = 0$$

This scheme is known to be very diffusive *i.e.* it smooths Shocks and discontinuities.

To obtain less numerical diffusion, we can consider a piecewise linear approximation like:

$$\frac{du_i}{dt} + \frac{f(u_{i+\frac{1}{2}}) - f(u_{i-\frac{1}{2}})}{\delta x} = 0$$

where

$$u_{i+\frac{1}{2}} := \frac{1}{2}(u_i + u_{i+1}), \quad u_{i-\frac{1}{2}} := \frac{1}{2}(u_{i-1} + u_i).$$

This scheme is more accurate but is oscillating (*i.e.* non TVD).

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#### ➡ SKIP: TVD Schemes

The total variation is defined by:

$$TV(u) = \sum_{i} |u_{i+1} - u_i|.$$

A scheme is said to be TVD (Total Variation Diminishing) if

$$rac{d}{dt}TV(u)\leq 0$$

or, after time discretization:

 $TV(u^{n+1}) \leq TV(u^n).$ 

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We can then use a MUSCL scheme:

$$\frac{du_i}{dt} + \frac{f_{i+\frac{1}{2}}^* - f_{i-\frac{1}{2}}^*}{\delta x} = 0$$

Numerical fluxes  $f_{i\pm\frac{1}{2}}^*$  correspond to a nonlinear combination of first and second order approximations of f(u).



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We define:

$$u_{i\pm\frac{1}{2}}^{*} = u_{i\pm\frac{1}{2}}^{L} (u_{i\pm\frac{1}{2}}^{L}, u_{i\pm\frac{1}{2}}^{R})$$

$$u_{i+\frac{1}{2}}^{L} = u_{i} + \frac{1}{2}\phi(r_{i})(u_{i+1} - u_{i})$$

$$u_{i+\frac{1}{2}}^{R} = u_{i+1} - \frac{1}{2}\phi(r_{i+1})(u_{i+2} - u_{i+1})$$

$$r_{i} = \frac{u_{i} - u_{i-1}}{u_{i+1} - u_{i}}$$

The function  $\phi$  is a slope limiter ensuring that the obtained solution is TVD, with

$$\phi(r) = 0$$
 if  $r \le 0$ ,  $\phi(1) = 1$ .

The literature contains a large variety of slope limiters. For instance the limiter minmod is defined by

$$\phi(r) = \max(0,\min(1,r)), \quad \lim_{r \to \infty} \phi(r) = 1.$$

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## **MUSCL** schemes for Euler equations

For a triangle  $T_i$ , we denote by  $B_i$  its centroid and by  $Q_{ij}$  the intersection of the segment  $[B_i, B_j]$  with the edge  $e_{ij}$  for all  $j \in \nu(i)$ .



We introduce the barycentric coordinates  $(\rho_{ij})_{j \in \nu(i)}$  by

$$\sum_{j\in\nu(i)}\rho_{ij}B_j=B_i,\quad \sum_{j\in\nu(i)}\rho_{ij}=1.$$

We assume that  $B_i$  is strictly in the interior of the triangle formed by the centroids of neighbour triangles. Thus  $\rho_{ij} > 0$ . We define the direction

$$t_{ij} = \frac{B_i B_j}{|B_i B_j|}$$

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We want now to reconstruct the values  $U_{ij}$  on the edge  $e_{ij}$ . Let v denote any component of U (piecewise constant). We define a first downwind slope by

$$p_{ij}^+ = rac{v_j - v_i}{|B_i B_j|} \quad \forall \ j \in 
u(i), \ 1 \le i \le n_T.$$

Therefore  $p_{ij}^{+}$  is an approximation of the derivative of v in the direction  $t_{ij}$ . The upwind slope is defined by:

$$\rho_{ij}^{-} = -\sum_{\substack{k \in \nu(i) \\ k \neq j}} \beta_{ijk} \rho_{ik}^{+} \quad \forall \ j \in \nu(i), \ 1 \le i \le n_T.$$

The slopes  $p_{ii}$  are then obtained by a limiter. For instance

$$p_{ij} := \operatorname{minmod}(p_{ij}^+, p_{ij}^-)$$

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 $v_{ij} := v_i + p_{ij} |B_i Q_{ij}|$ 

#### Remarks

- This reconstruction is exact for affine functions:  $v(Q_{ij}) = v_{ij}$  if v is piecewise linear
- The main advantage is that the reconstruction is typically 1-D. This enables using classical 1-D slope limiters.
- The property  $\rho_{ij} > 0$  implies  $\beta_{ijk} < 0$ . Therefore, if  $v_i$  is a local extremum, we have  $p_{ii}^+ \rho_{ii}^- \leq 0$ . Hence  $\rho_{ij} = 0$ . This means that extrema do not increase.
- For positivity reasons, the reconstruction must use physical variables and not conservative ones.

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## **Stationary radial solutions**

In order to test the numerical scheme, we construct a radial steady state solution of the equations: We look for a solution  $(u_r, u_\theta, u_z, p, e)$  that depends on r only and such that  $u_z = u_\theta = 0$ . We obtain the system:

$$\frac{d}{dr}(r\rho u_r) = 0$$
$$\frac{d}{dr}(r(\rho u_r^2 + \rho)) = \rho$$
$$\frac{d}{dr}(r u_r(e + \rho)) = 0$$
$$\rho = (\gamma - 1)\rho e$$

We deduce for  $\alpha, \beta \in \mathbb{R}$ 

$$rac{d
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$$\frac{d\rho}{dr} = \frac{\rho}{\left(\alpha\rho^2 r^2 - \frac{\gamma+1}{2(\gamma-1)}\right)(\gamma-1)r}, \qquad u_r = \frac{\beta}{\rho r}$$

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# Numerical tests

- A stationary radial solution
- Shock tube (SOD)
- (a) A supersonic flow in a channel

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# A stationary radial solution



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# Shock tube

Let  $\Omega$  denote the domain of parameters

 $\Omega = \{ (r, z); r \in [0, 1), z \in (0, 1) \}.$ 

We define  $\Omega_L = (0,1) \times (0,\frac{1}{2})$ ,  $\Omega_R = (0,1) \times (\frac{1}{2},1)$  and the initial conditions:

$$U(t=0) = egin{cases} U_L & ext{in } \Omega_L \ U_R & ext{in } \Omega_R \end{cases}$$

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### Shock tube: Test 1

We test a configuration with a left rarefaction wave, a contact discontinuity and a right shock wave. For this we prescribe:

$$\rho_L = 1, \ \rho_R = 0.125, \ u_L = u_R = 0, \ p_L = 1, \ p_R = 0.1$$



First Order: Rusanov and HLLC schemes: Mesh size 1/100

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First Order: Rusanov and HLLC schemes: Mesh size 1/200

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Second Order: Rusanov and HLLC schemes: Mesh size 1/100

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Second order: Rusanov and HLLC schemes: Mesh size 1/200

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## Shock tube: Test 2

We consider a configuration with a double shock and a contact discontinuity. This is obtained from the conditions:

$$\rho_L = \rho_R = 6$$
,  $u_L = 19.6$ ,  $u_R = -6.2$ ,  $p_L = 460$ ,  $p_R = 460$ 



Second order: Rusanov and HLLC schemes: Mesh size 1/200

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### Shock tube: Test 3

We now test a configuration with 2 rarefactions and a contact discontinuity and where the solution presents a vacuum like situation. This is obtained with the conditions:

$$\rho_L = \rho_R = 1, \quad u_L = -2, \quad u_R = 2, \quad p_L = 1, \quad p_R = 0.4$$



Second Order: Rusanov and HLLC: Mesh size 1/200

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# Supersonic flow in a channel

We consider a compressible Euler flow in a channel with an oblique obstacle (10 degrees) forming a cone.

Problem data:

$$P_{\infty} = 10^5 Pa, \ \rho_{\infty} = 1.16 Kg/m^3, M_{\infty} = 2$$

Mesh: 5176 triangles.

# **Cone: Density contours**



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## **Cone: Mach contours**



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